



Passive House Institute US

# LATENT LOADS, PSYCHOMETRICS, AND THE SENSIBLE HEAT RATIO

Lisa White, PHIUS Certification Manager

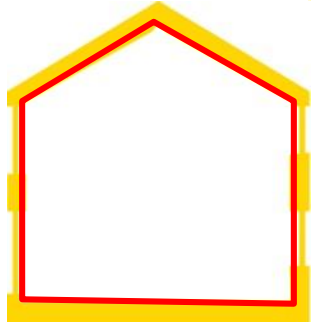
# AGENDA

1. BACKGROUND
2. PHUS+ 2015 COMPLIANCE
3. CAPABILITIES OF WUFI PASSIVE/PLUS
4. CHALLENGES OF HANDLING LATENT LOADS

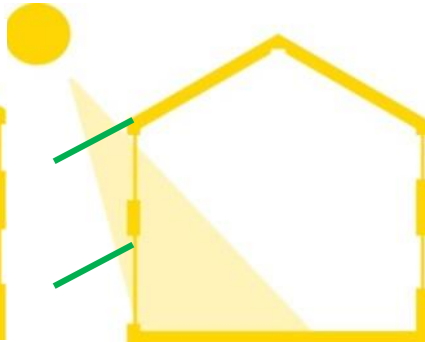
# PASSIVE BUILDING PRINCIPLES



CONTINUOUS  
INSULATION



AIR-TIGHT  
CONSTRUCTION



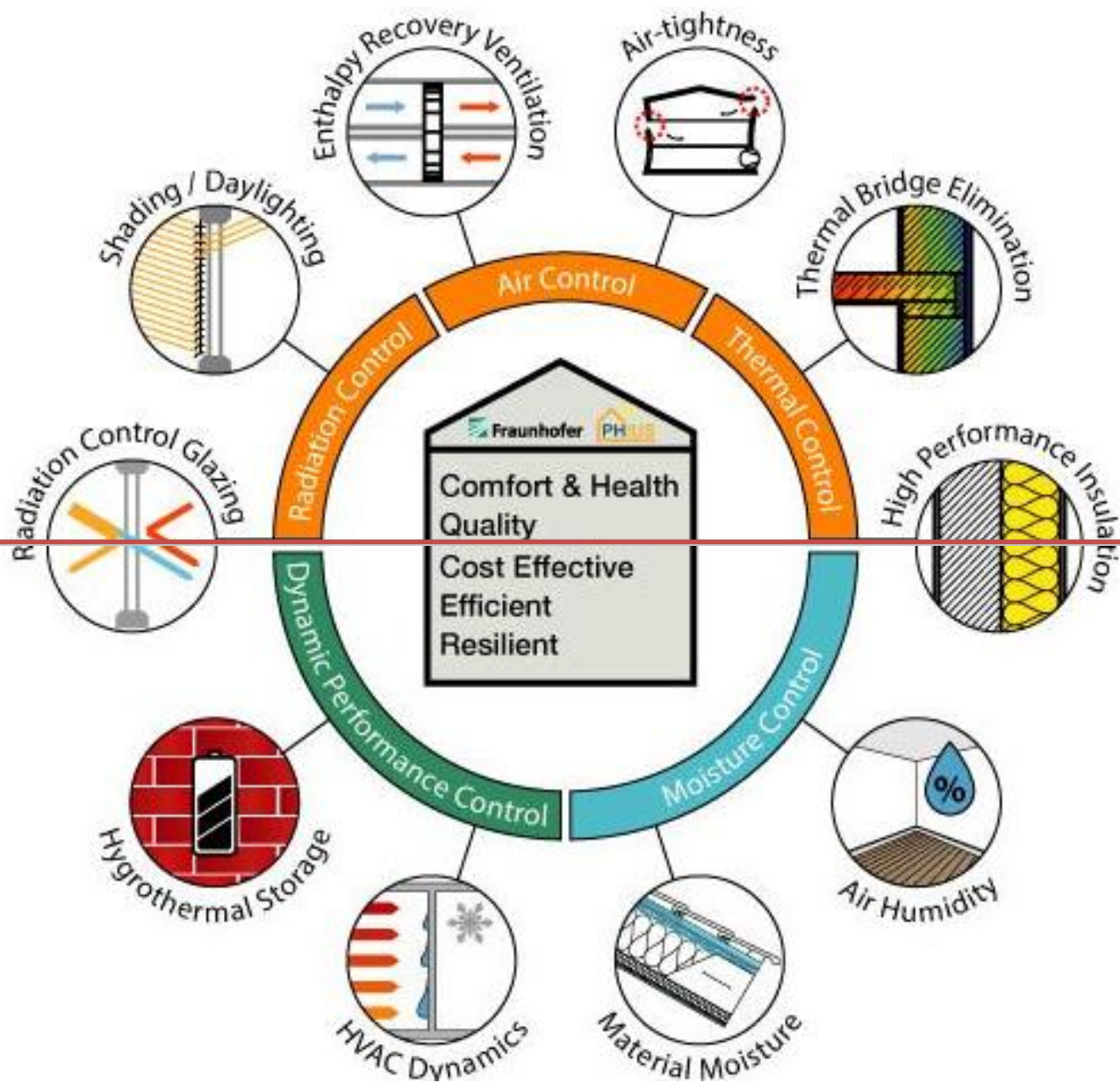
OPTIMIZED  
WINDOWS  
& SOLAR  
GAINS



BALANCED  
VENTILATION  
WITH HEAT  
RECOVERY



MINIMIZED  
MECHANICAL  
SYSTEMS





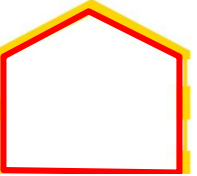



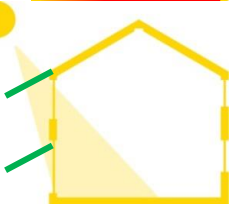











# DRIVERS OF LATENT LOADS

---

- Internal loads
- Occupants
- Exchange through opaque partitions
- Natural Ventilation
- Mechanical Ventilation
- Infiltration

		Heating Load	Sensible Cooling Load	Latent Cooling Load
	Continuous Insulation			
	Air-Tight Construction			
	Optimized Windows/Shading			
	Balanced Ventilation w/Heat & Moisture Recovery			

# RESULT OF APPLYING PASSIVE BUILDING PRINCIPLES:

SENSIBLE COOLING LOAD



LATENT COOLING LOAD



SENSIBLE HEAT RATIO



# SENSIBLE HEAT RATIO

$$= \frac{\textit{Sensible Cooling Load}}{\textit{Total Cooling Load}}$$

SHR = 1, No latent load

HIGH SHR = Low latent load  
relative to total load

LOW SHR = High latent load  
relative to total load



# VLI (Ventilation Load Index):

“the load generated by one cubic foot per minute of fresh air brought from the weather to space-neutral conditions over the course of one year”

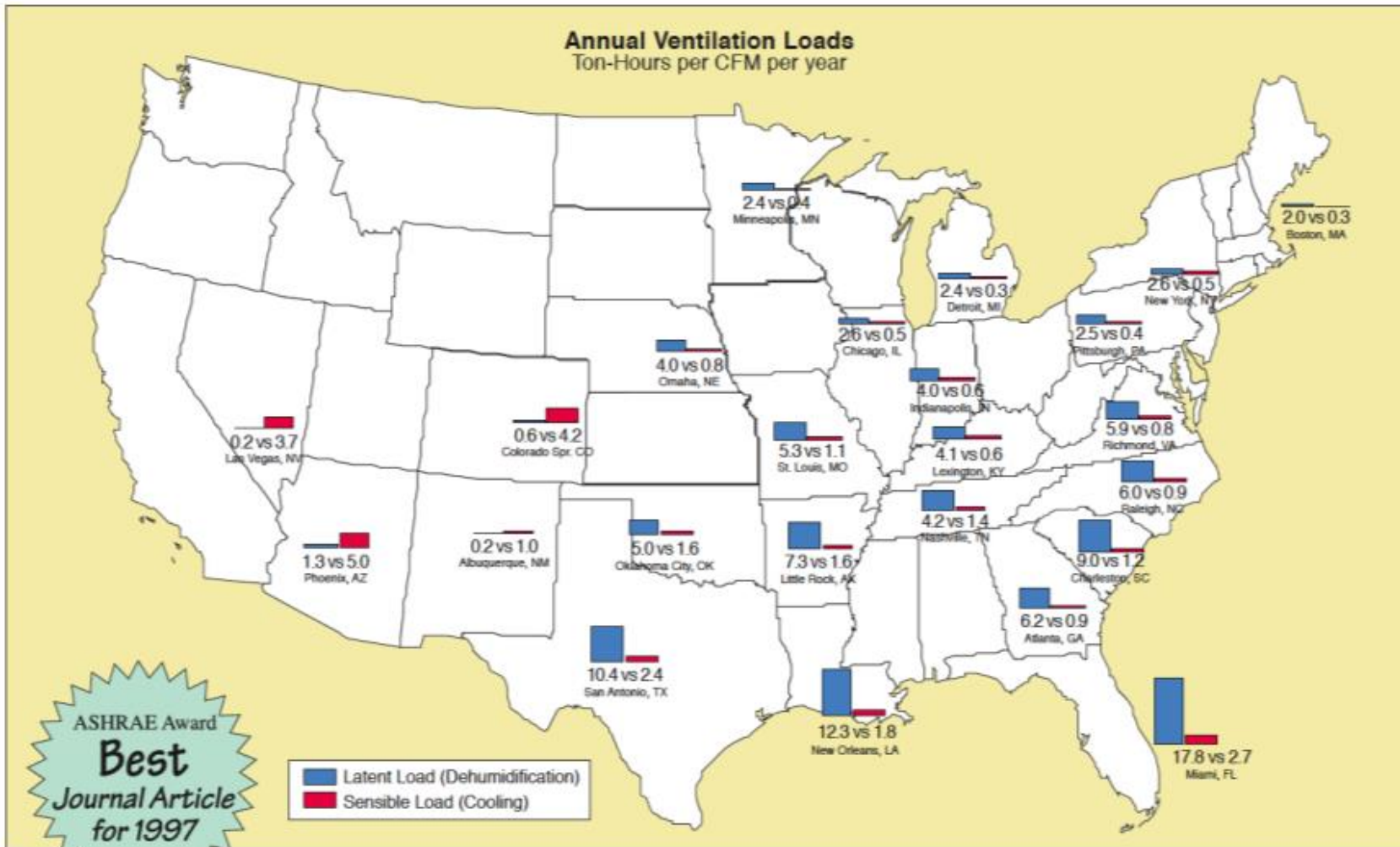


Fig. 1: Map of Ventilation Load Indexes (VLI) for selected continental U.S. locations

# VLI (Ventilation Load Index):

City	State	Ventilation Load Index (Ton-hrs/scfm/yr)		Total	Cumulative Load Ratio Latent:Sensible
		Latent	Sensible		
		Latent + Sensible			
Albuquerque	NM	0.2	1.0	1.2	0.2:1
Boston	MA	2.0	0.3	2.3	6.4:1
Detroit	MI	2.4	0.3	2.7	7.4:1
Minneapolis	MN	2.4	0.4	2.8	6.2:1
Pittsburgh	PA	2.5	0.4	2.9	5.8:1
New York	NY	2.6	0.5	3.1	5.1:1
Chicago	IL	2.6	0.5	3.1	5.0:1
Las Vegas	NV	0.2	3.7	3.9	0.04:1
Indianapolis	IN	4.0	0.6	4.6	6.6:1
Lexington	KY	4.1	0.6	4.7	7.4:1
Colorado Spr.	CO	0.6	4.2	4.8	0.1:1
Omaha	NE	4.0	0.8	4.8	5.3:1
Phoenix	AZ	1.3	5.0	6.2	0.3:1
St. Louis	MO	5.3	1.1	6.4	4.7:1
Oklahoma City	OK	5.0	1.6	6.6	3.2:1
Richmond	VA	5.9	0.8	6.7	7.2:1
Raleigh	NC	6.0	0.9	6.9	6.8:1
Atlanta	GA	6.2	0.9	6.9	6.7:1
Nashville	TN	6.2	1.4	7.6	4.6:1
Little Rock	AK	7.3	1.6	8.8	4.7:1
Charleston	SC	9.0	1.2	10.3	7.3:1
San Antonio	TX	10.4	2.4	12.8	4.4:1
New Orleans	LA	12.3	1.8	14.1	6.8:1
Miami	FL	17.8	2.7	20.5	6.7:1

# PsyCalc

Hours between

65°F DB

85°F DB

>65 gr/lb

Chicago, IL

1760 hours

20% of year!

**PsyCalc®** Hourly Data Binning and Statistics

North America | 659 | Elevation ft  
USA | 42.0 | Latitude North | Use External Data  
Illinois | 87.9 | Longitude West  
Chicago Ohare Intl Airport | Hide Stats

**Select Binning Type:**  
 Standard  
Bin on: Dry Bulb  
Bin size: 2  
 Joint Frequency  
Tdb size: 2  
W size: 2

**Select Months:**  
January July  
February August  
March September  
April October  
May November  
June December  
All Months | Clear Months

**# of Hours Selected** **8760**

**Create Bins**

**Weather Data Statistics for selected schedule:**

**Define selection criteria:**

	Equal or Above		Equal or Below
Dry Bulb Temperature °F	65.00	AND	85.00
		AND	
Humidity Ratio gr/lb d.a.	65.00	N.A.	70.00
		N.A.	
	50.00	N.A.	70.00
		N.A.	
	50.00	N.A.	70.00
		N.A.	

Get Stats | Export Stats

Stats for the selected hours fitting the selection criteria: Number of hours: 1760

Description	Units	Minimum	Maximum	Wt Average	Mean
Dry bulb temperature	°F	65.66	84.92	74.22	75.29
Dew point temperature	°F	54.30	78.72	64.23	68.67
Wet bulb temperature	°F	59.23	79.04	67.25	69.13
Humidity ratio	gr/lb	65.32	151.13	92.47	108.22
Relative humidity	%	37.08	100.00	71.71	68.54
Enthalpy	Btu/lb da	26.11	43.39	32.27	34.75
Wind speed	mph	0.00	26.40	9.62	13.20
Wind direction	degrees	0.00	360.00	173.70	180.00
Atmospheric pressure	psia	14.17	14.56	14.37	14.37

# PHIUS+ 2015

*Performance based standard  
with prescriptive requirements  
→ Concerned with both energy and  
comfort*

- 1. Defines infiltration limit*
- 2. Defines ventilation requirements*
- 3. WUFI Passive software used for compliance*



# AIR-TIGHTNESS

## *PHIUS+ 2015 Requirement*

### Acceptable Air Tightness of Walls in Passive Houses

Mikael Salonvaara and Achilles Karagiozis, Owens Corning

#### 1 Introduction

It has long been known that air-tightness is a critical element of a passive building, for two reasons. One is that super-insulation can only do so much to improve the energy performance of a building while the heat losses from air infiltration remain uncontrolled. The other is that air leaks can cause moisture problems / damage, and more-insulated assemblies are fundamentally more susceptible to such problems due to decreased heat flux, which lowers the rate of drying. (Nisson & Dutt 1985, LePage et al 2013)

When it comes to setting guidelines and standards for air-tightness, there has been a range of recommended performance thresholds, historically and in current practice. For example:

- 1-3 air changes per hour at 50 Pascals pressure difference (ACH50) in the detached house residential context (Nisson & Dutt 1985).
- 1.5-3 ACH50 (climate zone dependent) in the current DOE Zero Energy Ready Home requirements (rev. 05).
- 0.6 ACH50<sup>1</sup> under the standards of the Passivhaus Institut (PHI).
- 0.25 cfm at 75 Pascals pressure difference (cfm75) per ft<sup>2</sup> of enclosure (all 6 sides) in the U.S. Army Corps of Engineers protocol (version 3, 2012).
- 0.4 cfm75/ft<sup>2</sup> of enclosure in the U.S. General Services Administration P100 facilities standards (2015) at the "baseline" level, and 0.10 cfm75/ft<sup>2</sup> at the Tier 3 High Performance level.

The Air Barrier Association of America (ABAA) has set requirements for air barrier materials and assemblies. The air barrier materials should not have more than 0.004 cfm/ft<sup>2</sup> air leakage at 75 Pa and the air barrier assemblies (such as walls) should not leak more than 0.04 cfm/ft<sup>2</sup> at 75 Pa.

Consider how that translates into ACH50. Suppose a two-story home with 2400 square feet of conditioned floor area (exterior dimensions) • 27 feet wide, 44 feet long, and 18 feet high. The envelope area is then  $2 \cdot (27 \cdot 44 + 27 \cdot 18 + 44 \cdot 18) = 4932$  ft<sup>2</sup>. The interior air volume can be estimated as  $2 \cdot (25 \cdot 42 \cdot 8) = 16800$  ft<sup>3</sup>.

If the air barrier assemblies meet the ABAA definition, the leakage just through those assemblies would be  $0.04 \text{ cfm75/ft}^2 \cdot 4932 \text{ ft}^2 = 197 \text{ cfm75}$  or 11837 ft<sup>3</sup>/h. In terms of air changes per hour that is  $(11837 \text{ ft}^3/\text{h}) / (16800 \text{ ft}^3/\text{AC}) = 0.70 \text{ ACH175}$ .

<sup>1</sup> Based on interior air volume, rather than gross building volume.

0.05 CFM50/ft<sup>2</sup> envelope  
OR  
0.08 CFM75/ft<sup>2</sup> envelope

# SUMMARY OF VENTILATION REQUIREMENTS

## PHIUS+ Certification GuideBook v1.1

### 3.5.3 Ventilation

**The ventilation system must be capable of at least 0.3 ACH (based on the net volume) on its maximum setting.**

## PHIUS+ Single Family Quality Assurance Workbook v4.0

**1.11:** Rater-measured bathroom exhaust rates meets one of the following:  
>= 20cfm continuous OR 50 cfm intermittent

**1.13:** Rater-measured kitchen exhaust rates meets one of the following:  
>=25 cfm continuous, 100 cfm intermittent for range hoods, or 5ACH based on kitchen volume

### Balanced Ventilation Required

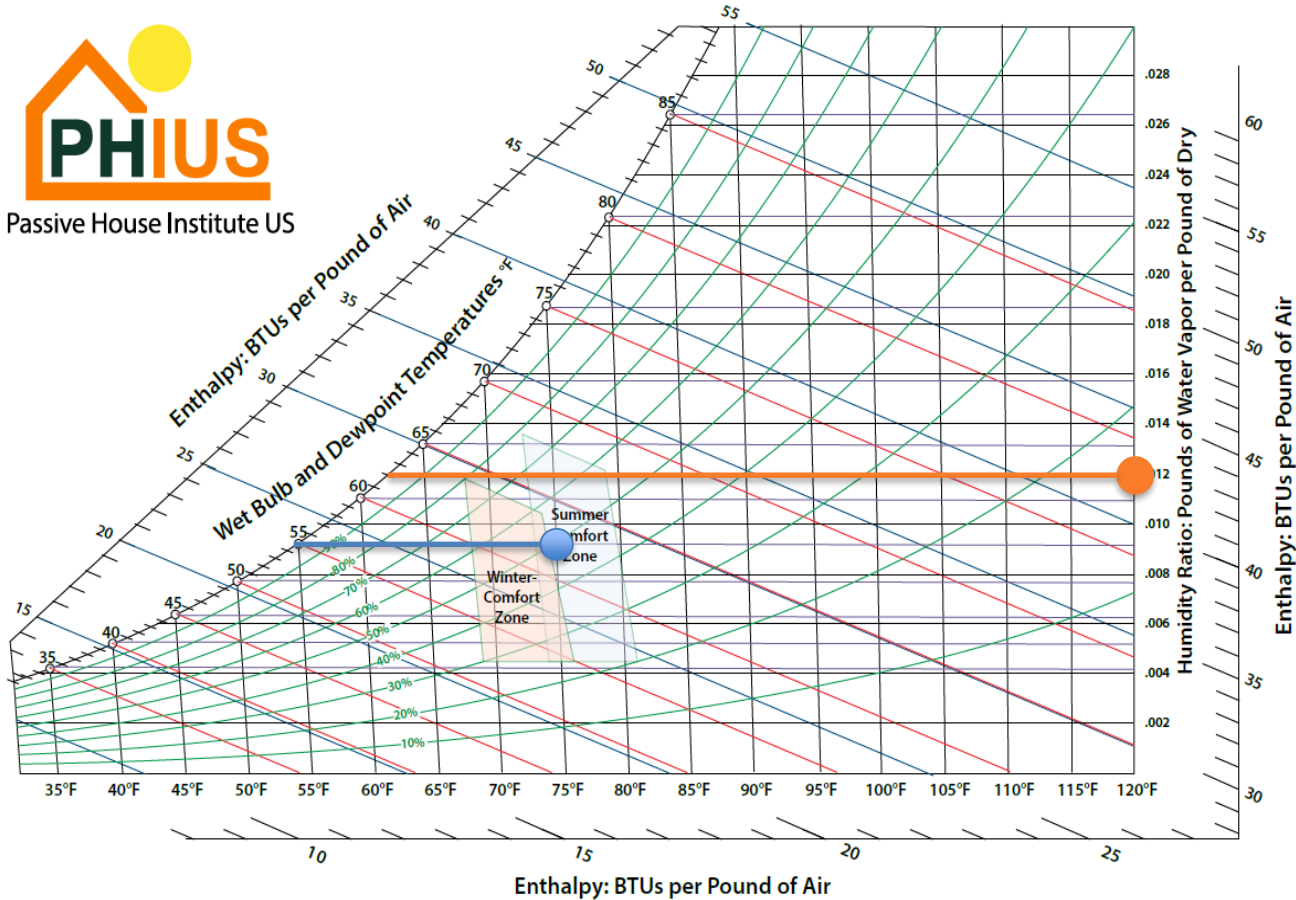
- Unbalanced has consequences for both energy modeling, building durability and IAQ
- Heat recovery is not required, or more than one fan necessarily, but air flow balance is required
- All air flow must be within 10% supply/exhaust, or below a 5 Pa pressurization / depressurization due to the whole-building ventilation.

# WUFI PASSIVE

*ANNUAL LATENT COOLING DEMAND (kBTU/ft<sup>2</sup>.yr)*

## *Influenced by:*

- *Natural ventilation (windows), day & night*
- *Mechanical ventilation*
  - *Includes latent recovery*
  - *Includes bypass/economizer mode*
- *Infiltration*
- *Maximum dehumidification ratio -- default = 0.012 lb/lb (can input different value)*
- *Internal sources – default value of 0.00041 lb/ft<sup>2</sup>.hr (can input different value)*



PHIUS SET-POINT FOR MAX DEHUMIDIFICATION RATIO IS 0.012 lb/lb  
(77F, 60% RH, 62F DP)

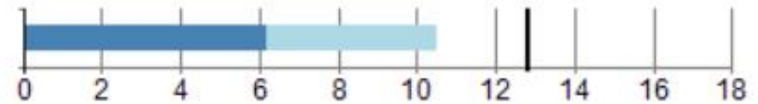
ASHRAE HANDBOOK HVAC APPLICATIONS – CHAPTER 62  
(75F, 50% RH, 55F DP)



## WUFI PASSIVE RESULTS WITH **0.012 lb/lb** MAX DEHUMIDIFICATION RATIO

### Cooling demand

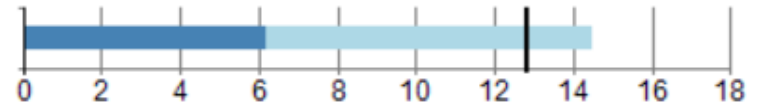
sensible:	<b>6.19</b>	kBtu/ft <sup>2</sup> yr
latent:	<b>4.3</b>	kBtu/ft <sup>2</sup> yr
specific:	<b>10.49</b>	kBtu/ft <sup>2</sup> yr
target:	<b>12.8</b>	kBtu/ft <sup>2</sup> yr
total:	31,923.96	kBtu/yr



## WUFI PASSIVE RESULTS WITH **0.009 lb/lb** MAX DEHUMIDIFICATION RATIO

### Cooling demand

sensible:	<b>6.19</b>	kBtu/ft <sup>2</sup> yr
latent:	<b>8.27</b>	kBtu/ft <sup>2</sup> yr
specific:	<b>14.46</b>	kBtu/ft <sup>2</sup> yr
target:	<b>12.8</b>	kBtu/ft <sup>2</sup> yr
total:	43,999.2	kBtu/yr



Latent cooling demand estimated almost 2x higher with new set-point!!

# WUFI PASSIVE

## MANUAL J - LATENT COOLING LOAD (kBTU/hr)

General Additional data Foundation interface **Manual J**

Manual J-residential cooling load calculation

**Climate / ventilation**

Outdoor design temperature [°F]	95
Indoor design temperature (optional) [°F]	77
Outdoor - Indoor moisture difference [%]	50
Air changes per hour [1/hr]	0.05
Altitude correction factor [-]	1

**Loads**

Nr.	Internal load	Quantity
1	Small Plant	6
2	Coffee maker - warmer	6
3	Dishwasher	6
4	Microwave	6

**Components**

Nr.	Name	Cooling load temperature difference [-]	Heat transfer multiplier [-]	Shade line multiplier [-]	Orientation	Area [ft²]	U-value [Btu/hr ft² °F]
1	Z.1. C. 1	10			S (34 %), E (18 %), W (15 %), N	6163.6	0.0282
2	Z.1. C. 2	5			Horizontal (100 %)	3116	0.019
3	Z.1. C. 3	5			Horizontal (100 %)	3116	0.0481
4	Z.1. C. 4: (SOUTH, Floor 2, Fixed)		1	0.6	S (100 %)	65.5	0.1572
5	Z.1. C. 5: (SOUTH, Floor 1, Fixed)		1	0.6	S (100 %)	65.5	0.1572
6	Z.1. C. 6: (SOUTH, Floor 1, Casement)		1	0.6	S (100 %)	81.5	0.1651

**Results**

Name	Sensible Cooling [Btu/hr]	Latent cooling load [Btu/hr]
Opaque components	2781.3	0
Fenestration	3363.5	0
Ventilation	6472.7	11114.8
Internal loads	18004.1	9210
Infiltration	1051.2	1805.2
<b>Total</b>	<b>31672.9</b>	<b>22130</b>

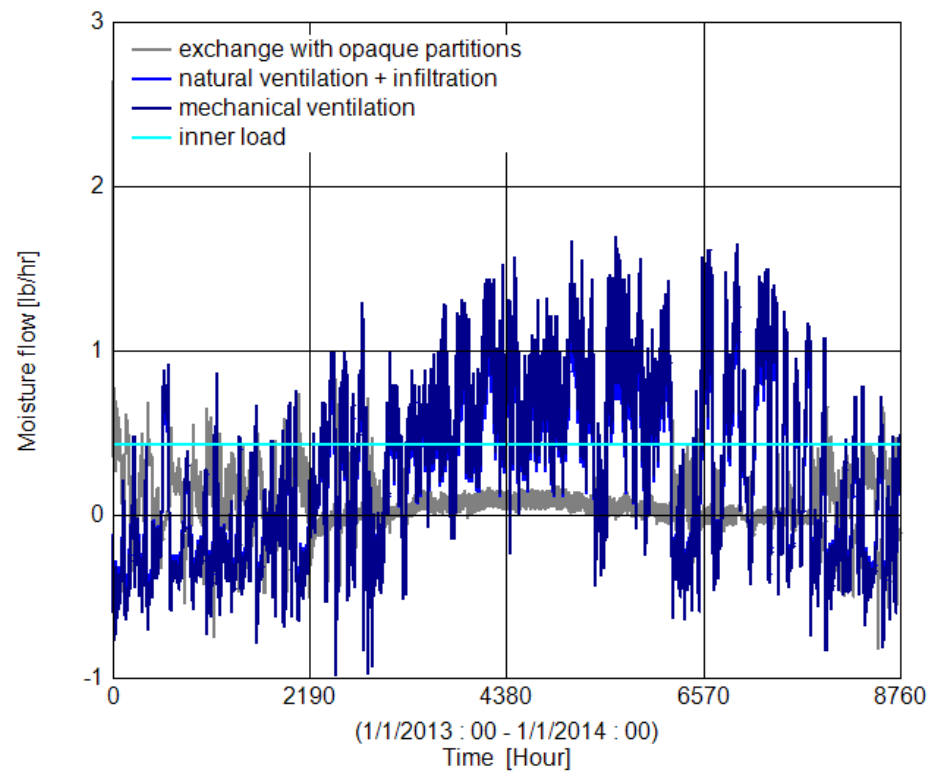
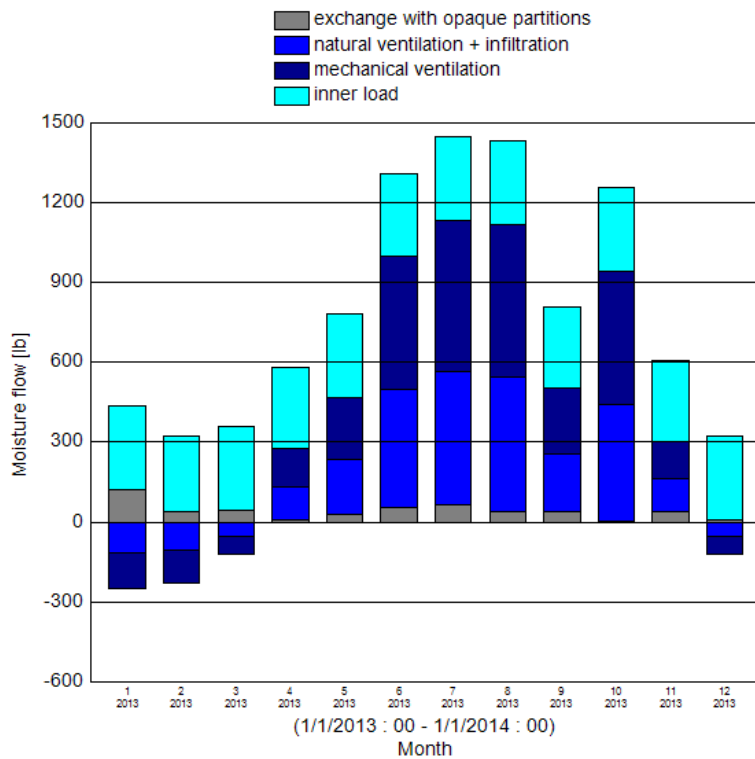
**Interim results**

Cooling temperature difference [°F]	50
Average air change rate [1/hr]	1.5
Altitude building [ft]	610

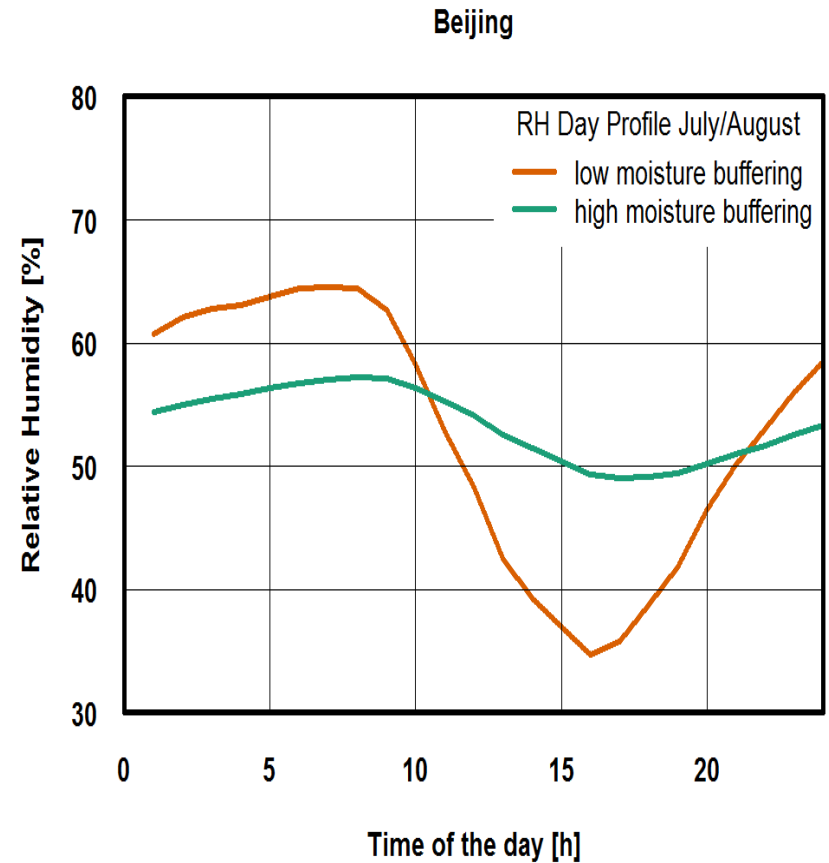
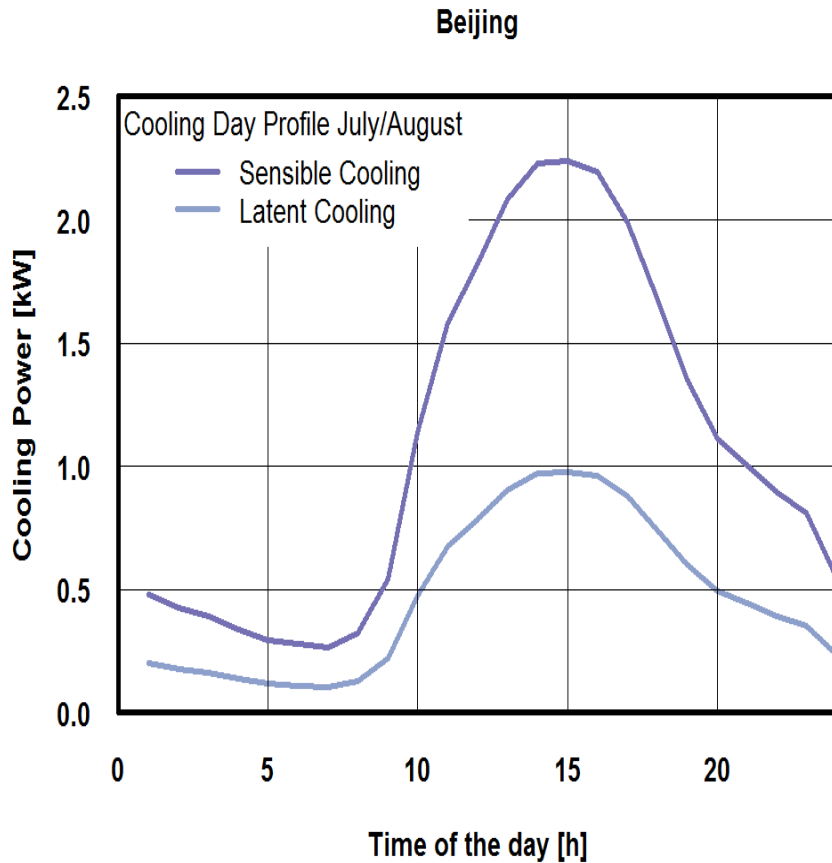
Status: OK

# WUFI PASSIVE – Dynamic (WUFIplus)

## Abbate Case Study – Austin, TX Moisture Flows



# Moisture Buffering Effect on Daily RH Fluctuations



Moisture buffering capacity of the envelope dampens daily indoor RH cycles

# CHALLENGES WITH COMPLIANCE WITH PHIUS+ 2015 *IN HOT/HUMID CLIMATES*

- 1) Dehumidify to lower RH = increased source energy use*
- 2) Ventilating dehumidifier = difficult meeting heating demand & heating load targets for PHIUS+ 2015 without balanced ventilation with heat recovery*



	Water Removal*	Current Draw	Efficiency	Energy Factor	Sized For	Air Filter	Dimensions	Weight
<b>Ultra-Aire 70H</b>	70 pints per day	5.1 amps	5.0 pints per kWh	2.4 L per kWh	Up to 1,800 Sq. Ft.	MERV-11	12"W 12"H 28"L	55 lbs
<b>Ultra-Aire 98H</b>	98 pints per day	5.9 amps	6.1 pints per kWh	2.95 L per kWh	Up to 2,300 Sq. Ft.	MERV-11	14.5"W 19.5 H 32.375"L	81 lbs
<b>Ultra-Aire 100V</b>	110 pints per day	6.4 amps	6.2 pints per kWh	3.0 L per kWh	Up to 2,500 Sq. Ft.	MERV-11	21"W 49"H 17"L	119 lbs
<b>Ultra-Aire XT105H</b>	105 pints per day	4.9 amps	8.8 pints per kWh	4.2 L per kWh	Up to 2,500 Sq. Ft.	MERV-11	20.25"W 21.75"H 41.5"L	140 lbs
<b>Ultra-Aire XT155H</b>	155 pints per day	8.0 amps	7.3 pints per kWh	3.4 L per kWh	Up to 3,500 Sq. Ft.	MERV-11	20.25"W 21.75"H 41.5"L	140 lbs
<b>Ultra-Aire XT205H</b>	205 pints per day	13.2 amps	5.7 pints per kWh	2.7 L per kWh	Up to 5,000 Sq. Ft.	MERV-11	20.25"W 21.75"H 41.5"L	140 lbs
<b>Ultra-Aire SD12</b>	184 pints per day	<b>Dehumidifier:</b> 1.4 amps <b>Condenser:</b> 9.7 amps	6.6 pints per kWh	3.1 L per kWh	Up to 4,000 Sq. Ft.	MERV-11	<b>Dehumidifier:</b> 20.25"W 21.75"H 41.5"L <b>Condenser:</b> 10"W 25.5"H 33"L	<b>Dehumidifier:</b> 110 lbs <b>Condenser:</b> 75 lbs

The Ultra-Aire SD12 also provides 4,300 BTUs/Hour of Sensible Cooling



XT PATENTS: D570,988; 8,069,681; 9,052,132

\*at 80°F and 60% RH  
Rev 1/5/16

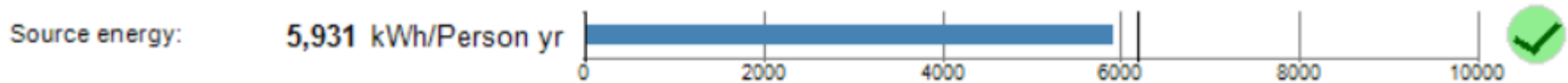
**Best Unit:**  
4.2 L/kWh  
(8.8 pints/kWh)  
= COP 2.6!

Most other high performance units with COP ~1.5-2

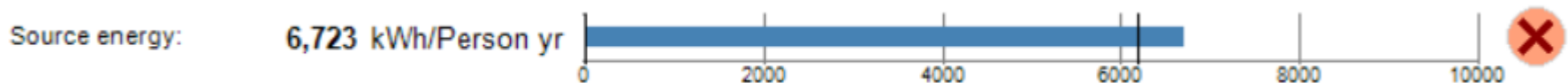
For heating equip: equivalent to HSPF ~8

For sensible cooling: equivalent SEER ~12

WUFI PASSIVE RESULTS WITH **0.012 lb/lb** MAX DEHUMIDIFICATION RATIO



WUFI PASSIVE RESULTS WITH **0.009 lb/lb** MAX DEHUMIDIFICATION RATIO



# CHALLENGES OF AVAILABLE EQUIPMENT

1. AIR CONDITIONING UNITS NOT DESIGNED FOR LOW SENSIBLE HEAT RATIO
2. MOST COOLING SYSTEMS ONLY CONTROLLED BY DRY BULB
3. LIMITED EFFICIENCY OF MOISTURE REMOVAL /DEHUMIDIFICATION
4. LIMITED ERV LATENT RECOVERY EFFICIENCY

# COMMON MISCONCEPTIONS

1. “ERV IS A DEHUMIDIFIER”
2. “VRF IS THE MAGIC BULLET FOR ALL SYSTEMS DESIGN”
3. “FULL DEHUMIDIFICATION LOAD CAN BE SATISFIED BY SLOWING DOWN SUPPLY AIRFLOW RATE”



# WHAT WE NEED

- 1). An affordable, efficient, reliable, simple mechanical system solution that handles latent loads (ideally before introduced to the space).
- 2). Awareness and capability of AC systems to control latent loads
- 3). Re-think ventilation strategies and requirements?
- 4). WUFI Passive integrated calculation for latent cooling load and output of SHR
- 5). Deeper understanding of potential of hygric buffering



# WHAT ARE THE SOLUTIONS??