

# A Comparison of the NFRC and CEN Thermal Transmittance Calculation Methods in North America's Eight Climate Zones

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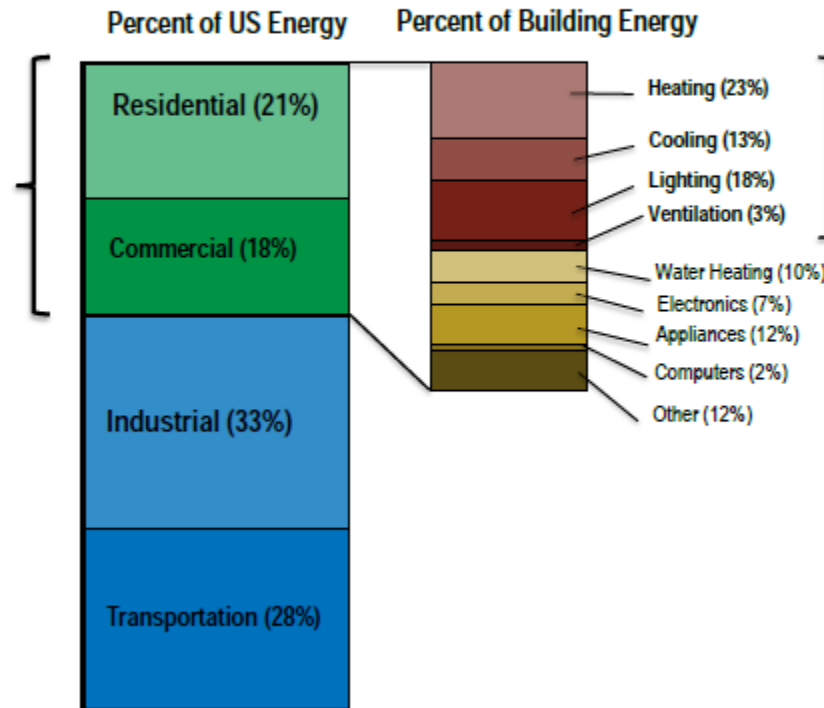
# Introduction

- ▶ Residential sector, 3<sup>rd</sup> largest consumer of energy in Canada, consuming 17% of the total energy used and producing 15% of total GHGs (NRC, 2009)
- ▶ In a typical home, 30–50% of the energy used is transmitted through the windows (Gustavsen, Grynninga, Arasteh, Petter Jelle, & Goudey, 2011)
- ▶ Window frames account for 20 to 30% of the whole window area yet can be responsible for more than 30% of the rate of heat transfer (Gustavsen, Arasteh, Petter Jelle, & Curcija, 2008)

# Energy Consumption of Windows in the U.S., 2011

## Why worry about windows?

Buildings are responsible for about 40% of US primary energy consumption



Over 58% of the energy used in a building falls in an end use impacted by windows

# Canadian and American Window Ratings (National Fenestration Rating Council (NFRC))



 National Fenestration Rating Council® <b>CERTIFIED</b>	<b>World's Best Window Co.</b> Series "2000" Casement Vinyl Clad Wood Frame Double Glazing • Argon Fill • Low E ABC-X-1-00001-00001	
	<b>ENERGY PERFORMANCE RATINGS</b>	
U-Factor <b>0.35</b> (U.S./I-P)	U-Factor <b>1.99</b> (Metric/SI)	Solar Heat Gain Coefficient <b>0.32</b>
<b>ADDITIONAL PERFORMANCE RATINGS</b>		
Visible Transmittance <b>0.51</b>	Air Leakage <b>0.2</b> (U.S./I-P)	Air Leakage <b>1.0</b> (Metric/SI)
Condensation Resistance <b>51</b>	—	
<small>Manufacturer stipulates that these ratings conform to applicable NFRC procedures for determining whole product performance. NFRC ratings are determined for a fixed set of environmental conditions and a specific product size. NFRC does not recommend any product and does not warrant the suitability of any product for any specific use. Consult manufacturer's literature for other product performance information. www.nfrc.org</small>		

Windows				
Zone	Heating Degree-Day Range	Compliance Paths		
		Energy Rating (ER)	or	U-Factor
		Minimum ER (unitless) Maximum U-Factor 2.00 W/m <sup>2</sup> •K (0.35 Btu/h•ft. <sup>2</sup> •°F)		Maximum U-Factor W/m <sup>2</sup> •K (Btu/h•ft. <sup>2</sup> •°F)   Minimum ER (unitless)
A	≤ 3500	21	or	1.80 (0.32)   13
B	> 3500 to ≤ 5500	25	or	1.60 (0.28)   17
C	> 5500 to ≤ 8000	29	or	1.40 (0.25)   21
D	> 8000	34	or	1.20 (0.21)   25

$$U_t = \frac{[\sum(U_f A_f) + \sum(U_e A_e) + \sum(U_c A_c)]}{A_{pf}}$$

# European Committee for Standardization (CEN)

## Certificate

valid until 31.12.2011

**Component suitable for Passive Houses: Window Frame**

**Manufacturer: Vale Passive Window Partnership Ltd. Pembrokeshire SA41 3TH**

**Name of product: The Vale Passive Window**

**The following criteria were checked to award the certificate:**  
The criteria are valid for the cool temperate climate.

Passive House comfort criterion:  
Under standard conditions (use of glazing with  $U_g = 0.7 \text{ W/(m}^2\text{K)}$ , width of window 1.23 m, height of window 1.48 m) the U-Value of the window fulfils the following condition:

**$U_w = 0.79 \leq 0.80 \text{ W/(m}^2\text{K)}$**

Thermal data of the window frame:

Frame	jamb	parapet	Spacer	Swisspacer V
$U_f$ [W/(m <sup>2</sup> K)]	0.77	0.80	$\Psi_g$ [W/(mK)]	0.028
Width [mm]	128	128		

Conditions specific for Passive Houses:  
The suitability for Passive Houses was checked only with the spacer denoted above; thermally worse spacers, especially those made of aluminium, lead to significantly higher thermal losses.

Installing the window suitable for Passive House:  
Including all thermal bridge effects, the window fulfils the condition

**$U_{w,installed} \leq 0,85 \text{ W/(m}^2\text{K)}$**

If the window is installed into wall constructions suitable for Passive Houses (brick wall with thermal insulation, light weight wooden construction and form work for concrete of polystyrene) according to the drawings of details given in the appendix.

**The certificate has to be used as follows:**

**Component suitable for Passive Houses**  
Dr. Wolfgang Feist

**Window frame:**  
 $U_f = 0.77 / 0.80 \text{ W/(m}^2\text{K)}$   
 $\Psi_g = 0.028 \text{ W/(mK)}$   
Width = 128 / 128 mm

Passivhaus Institut  
Dr. Wolfgang Feist  
Rheinstraße 44/46  
D-64283 Darmstadt

### Datenblatt zum Zertifikat

Rahmenschritt 'unten'      Isothermen- und Wärmestrombild

**Vale Passive Window Partnership 'The Vale Passive Window'**

Fensterrahmen aus gedämmten Holzprofilen; Holzanteile des Rahmens aus Lärche mit einer Rohdichte  $\rho = 600 \text{ kg/m}^3$  und  $\lambda = 0,15 \text{ W/(mK)}$ ; Dämmung aus Polyurethan-Hartschaum mit  $\lambda = 0,048 \text{ W/(mK)}$  und Polyurethan-Recyclingmaterial mit  $\lambda = 0,09 \text{ W/(mK)}$

Verglasung <sup>1)</sup> 44 mm (4/16/4/16/4)

		seitl./oben	unten
Rahmenkennwerte	$U_f$ [W/(m <sup>2</sup> K)]	0,77	0,80
	Ansichtsbreite [mm]	128	128
Abstandhalter: 'Swisspacer V'	$\Psi_g$ [W/(mK)]		0,028
Temperaturfaktor am Glasrand	$f_{Ra=0,20 \text{ mK/W}}$ [-]		0,79
Fenster-U-Wert <sup>1)</sup> (1,23 x 1,48 m)	$U_w$ [W/(m <sup>2</sup> K)]		0,79 <sup>1)</sup>

Hersteller: Vale Passive Window Partnership Ltd.  
c/o Thomas Joinery Bancyfynnon, Brynberian, Crymch,  
Pembrokeshire SA41 3TH

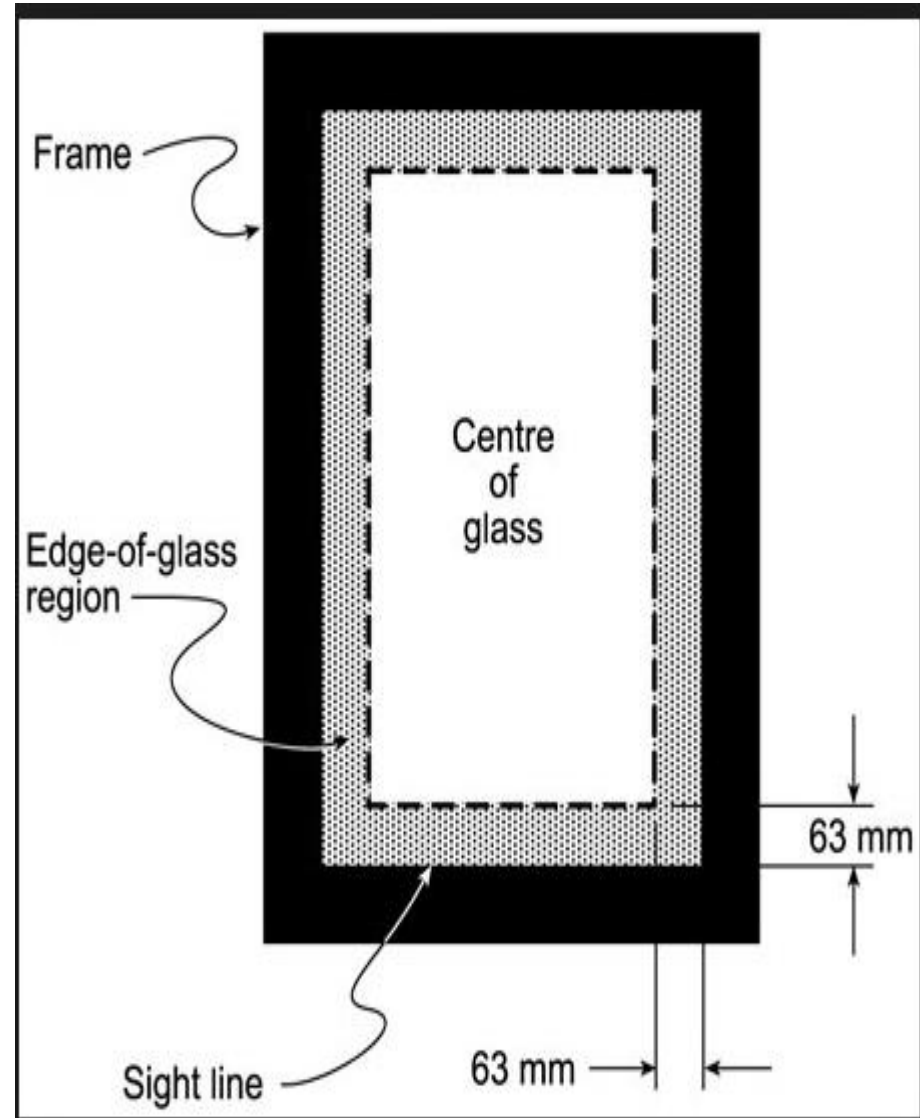
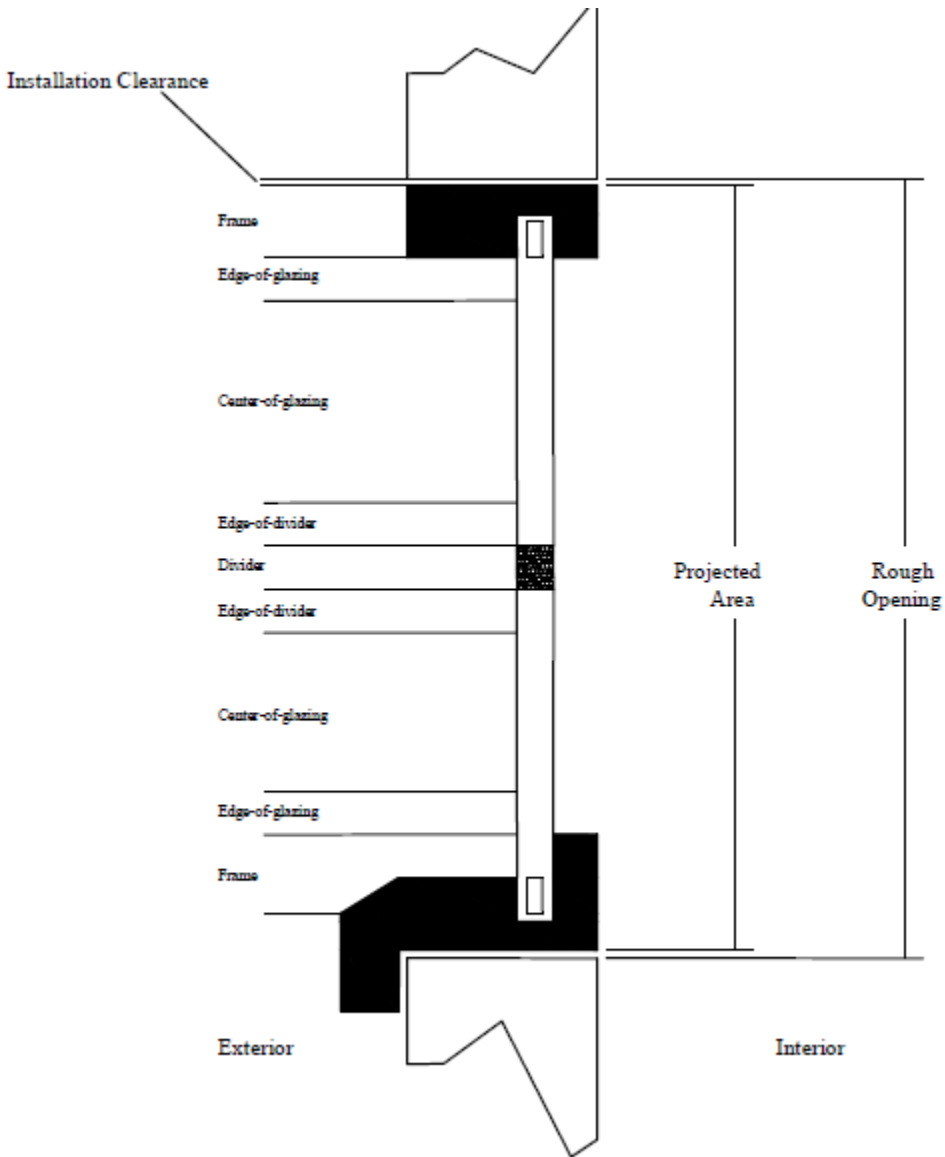
Berechnung: Passivhaus Institut 2010

<sup>1)</sup> Bei der Ermittlung des Fenster-U-Wertes (b = 1,23 m, h = 1,48 m) wurde ein Glas-U-Wert  $U_g = 0,70 \text{ W/(m}^2\text{K)}$  angesetzt.

$$U_w = \frac{\sum A_g U_g + \sum A_f U_f + \sum l_g \Psi_g}{\sum A_g + \sum A_f}$$

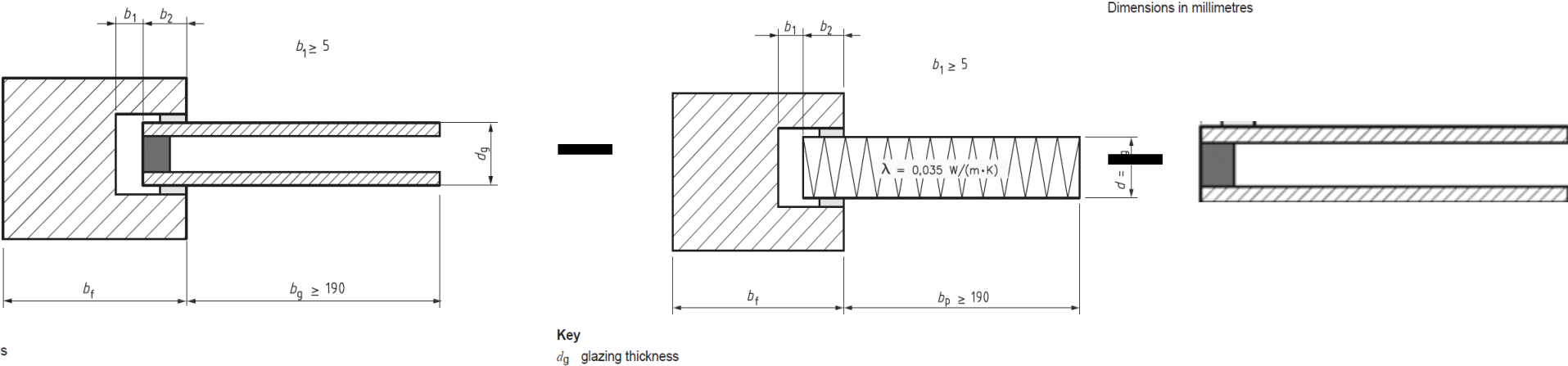
# North American (NFRC) and European (CEN) Window Energy Performance Standards

- ▶ Long disagreement between both methods;  
+ / - 10% difference (Blanusa, 2001 and Weitzmann et al., 2000)
  - Calculation methods
  - Interior and exterior temperatures
  - Surface film coefficients
  - Wind velocities
  - Edge effects



(NFRC, 2010)

# $\psi$ -Value (CEN)

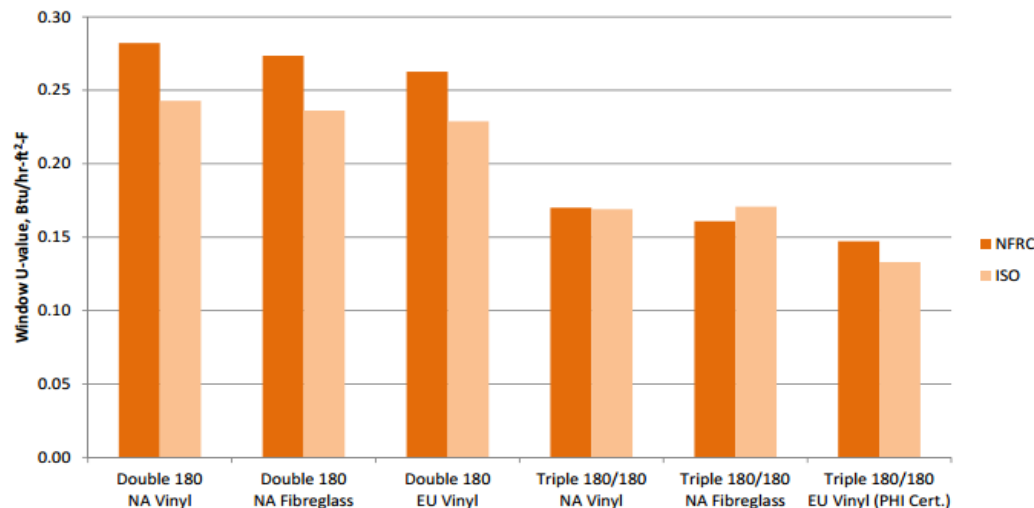


$$\psi = L_{\psi}^2 D - U_f b_f - U_g b_g$$



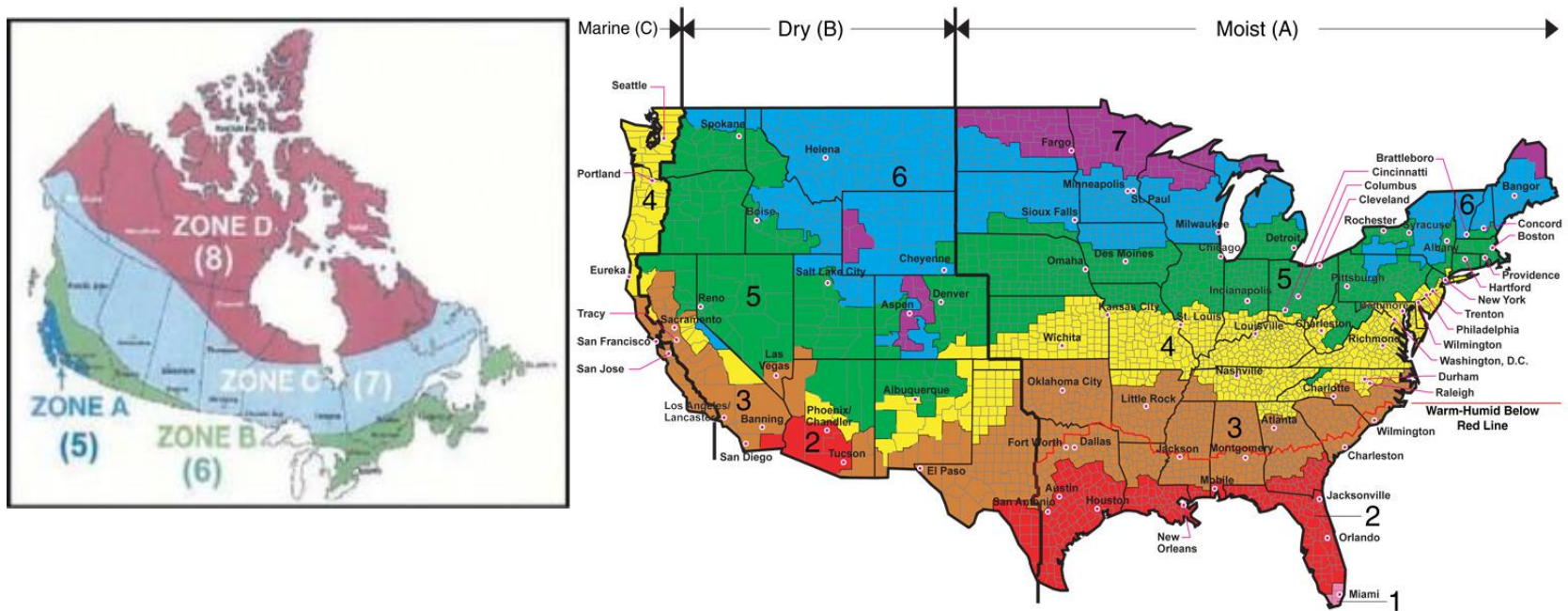
# U<sub>window</sub>: NFRC VS CEN

- NFRC center-of-glass U-values: up to 23% higher than CEN values
- NFRC frame U-values: 5% lower to 24% higher than CEN values
- NFRC whole window U-values: 14% lower to 18% higher than CEN values



(RDH Building Engineering Ltd., 2014)

# North America's 8 Climate Zones (IECC/ASHRAE)



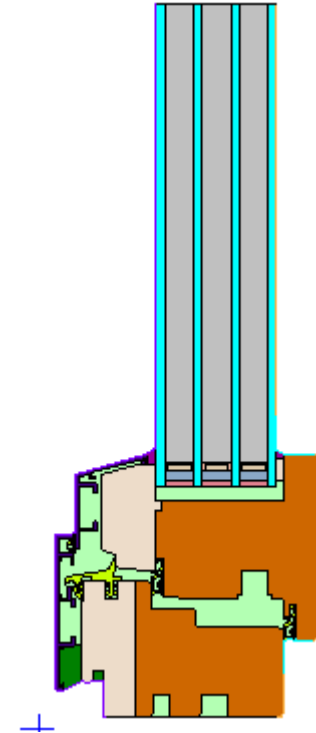
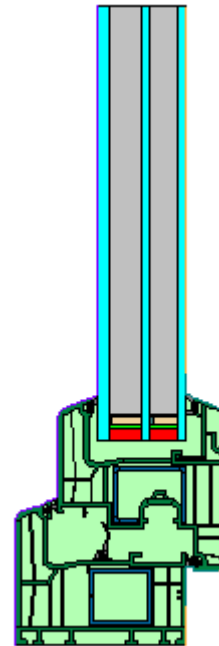
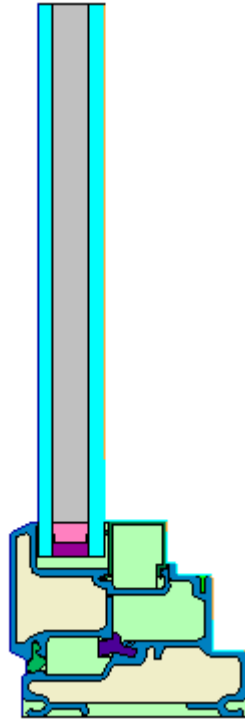
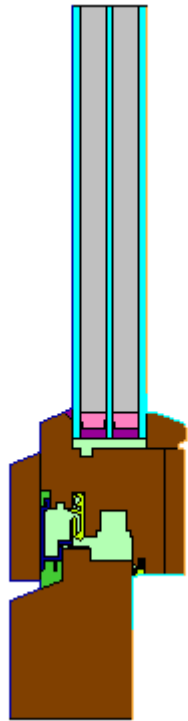
All of Alaska in Zone 7 except for the following Boroughs in Zone 8: Bethel, Dellingham, Fairbanks, N. Star, Nome North Slope, Northwest Arctic, Southeast Fairbanks, Wade Hampton, and Yukon-Koyukuk

Zone 1 includes: Hawaii, Guam, Puerto Rico, and the Virgin Islands

# Research Questions

1. What are the differences between the NFRC and CEN calculation methods for determining the U-value for window products?
2. What parameters can be harmonized between the two U-value calculation methods?
3. How are these parameters affected by the different boundary conditions in North America's eight climate zones?

# Methodology



# Simulation Matrix

Exterior Temp.	Frame Material	Glazing Combination	Spacer	Material Thermal Conductivity	Frame Cavity Method	Wind Speed	Surface Film Coefficients	SHGC Methods
NA 8 climate zones	Insulated fiberglass	Double IGU; high and low SHGC	A	NFRC 101	NFRC	Inland	NFRC	NFRC
	Solid wood	Triple IGU; high and low SHGC	B	CEN (ISO 10077-2)	CEN	Coastal	CEN	CEN
	TBSW	Quad IGU; high SHGC	C					
	U-PVC							

# NFRC and CEN Winter Boundary Conditions

	North America (NFRC)	Europe (CEN)
ISO Standard Used	ISO 15099	ISO 10077
Interior Temperature	21°C	20°C
Exterior Temperature	-18°C	0°C
Exterior Wind Velocity	5.5 m/s	4 m/s
Exterior Radiant Mean Temperature	$T_{r,m} = T_{\text{exterior}}$	$T_{r,m} = T_{\text{exterior}}$
Interior Radiant Mean Temperature	$T_{r,m} = T_{\text{interior}}$	$T_{r,m} = T_{\text{interior}}$

# NFRC and CEN Summer Boundary Conditions

	NFRC	CEN
Standard	NFRC 200-2010	ISO 15099
Interior temperature	24°C	25°C
Exterior temperature	32°C	30°C
Interior convective surface heat transfer coefficient, $h_{c, int}$	7.7 W/(m <sup>2</sup> K) (NFRC 102 $h_{c, int}$ and ASTM E1423)	2.5 W/(m <sup>2</sup> K)
Exterior convective surface heat transfer coefficient, $h_{c, ext}$	15 W/(m <sup>2</sup> K)	8 W/(m <sup>2</sup> K)
Radiant Mean Temperature, $T_{r, m}$	$T_{ex}$	$T_{ex}$
Solar irradiance, $I_s$	783 W/m <sup>2</sup>	500 W/m <sup>2</sup>
Wind Velocity	2.75 m/s	4 m/s

(Chen and Wittkopf, 2011)

# NA's Climate Zone Boundary Conditions

(ASHRAE, 2009)

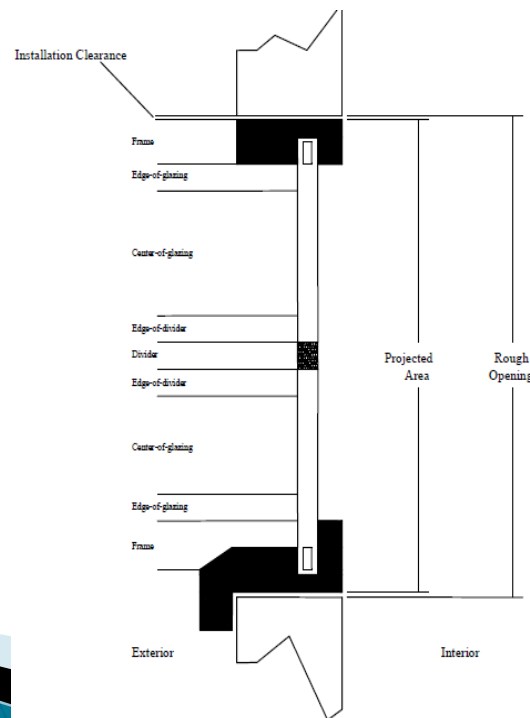
Climate Zones (inland)	Winter Design Temp. (°C)	Summer Design Temp. (°C)	Annual Low Average Temp. (°C)	Annual Average Temp (°C)	Annual High Average Temp. (°C)	Wind Velocity (m/s)
1 **						
2 Austin, TX	-1	37	14.4	20.3	26.2	7.6
3 Atlanta, GA	-4	33	11.8	17.0	22.2	7.7
4 Albuquerque, NM	-6	34	7.5	14.0	20.4	9.3
5 Indianapolis, IN	-14	32	6.6	11.8	16.9	8.4
6 Toronto, ON	-16	29	5.6	9.2	12.7	9.1
7 Winnipeg, MB	-30	29	-3.1	2.6	8.3	9.8
8 Yellowknife, NT	-40	24	-9	-4.6	-0.2	7.7

Climate Zones (coastal)	Winter Design Temp. (°C)	Summer Design Temp. (°C)	Annual Low Average Temp. (°C)	Annual Average Temp. (°C)	Annual High Average Temp. (°C)	Wind Velocity (m/s)
1 Miami, FL	11	33	21.2	25.1	29.1	7.7
2 Jacksonville, FL	0	34	14.3	20.3	26.3	7.3
3 San Francisco, CA	5	26	10.6	14.1	17.6	10.6
4 New York City, NY (JFK airport)	-8	30	8.3	12.3	16.2	9.6
5 Vancouver, BC	-4	24	6.5	10.1	13.7	7.6
6 St. John's, NFLD	-14	23	0.6	4.7	8.7	12.3
7 Whitehorse, YT	-35	23	-5.9	-0.7	4.5	8.4
8 Iqaluit, NU	-38	14	-13.6	-9.8	-6.0	11.1

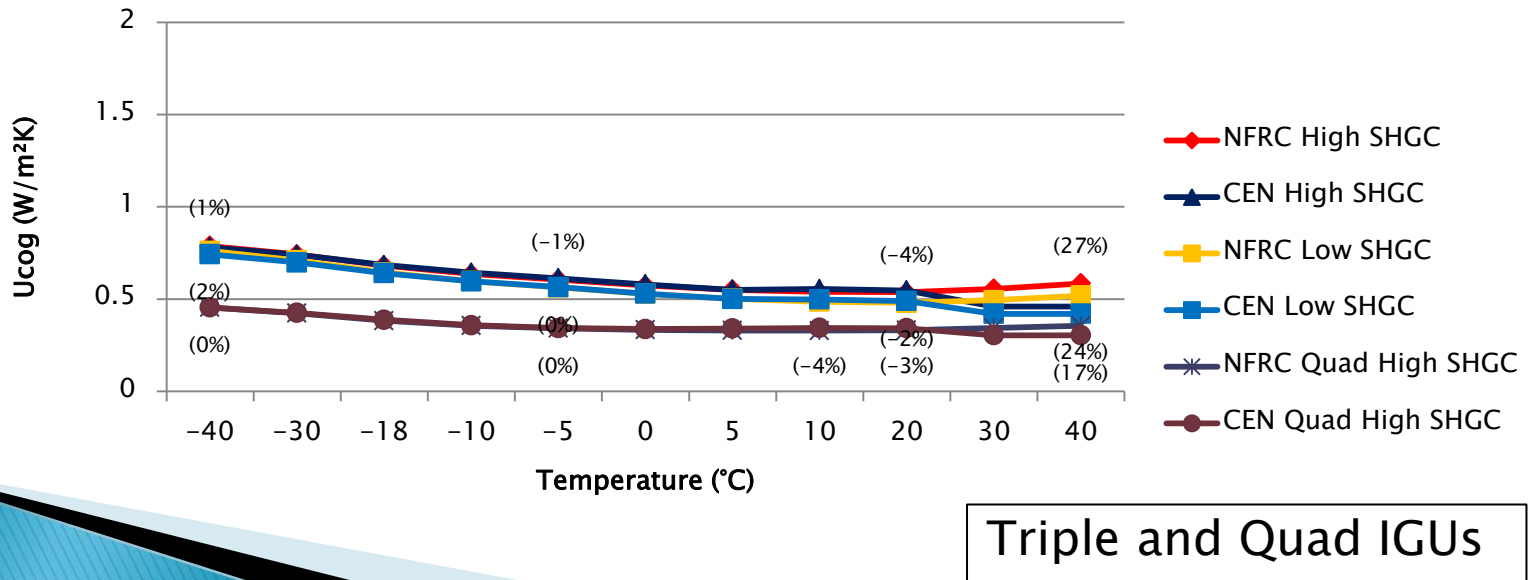
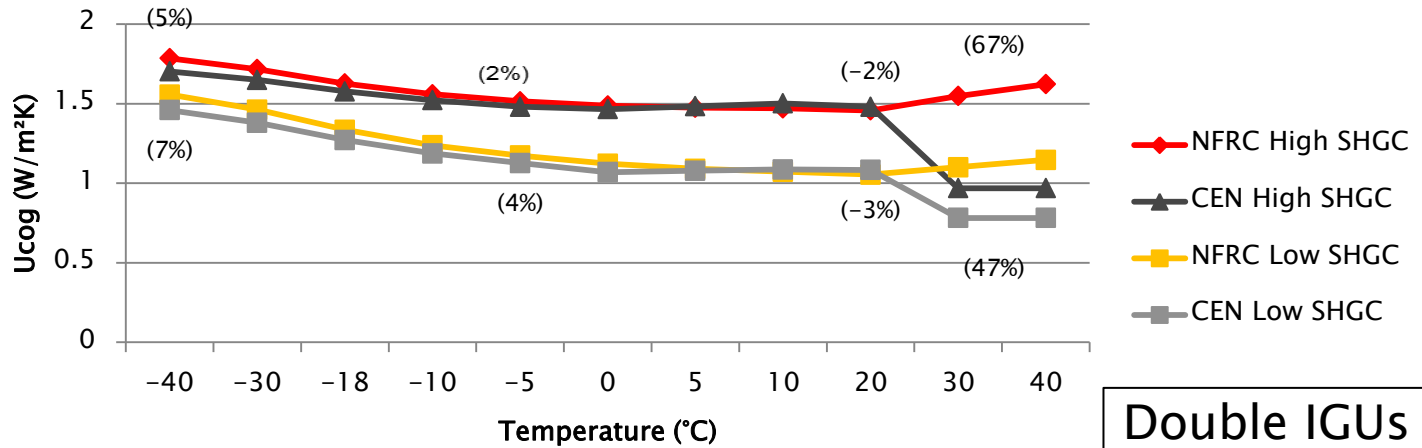


# RESULTS: Solar Heat Gain Coefficient (SHGC)

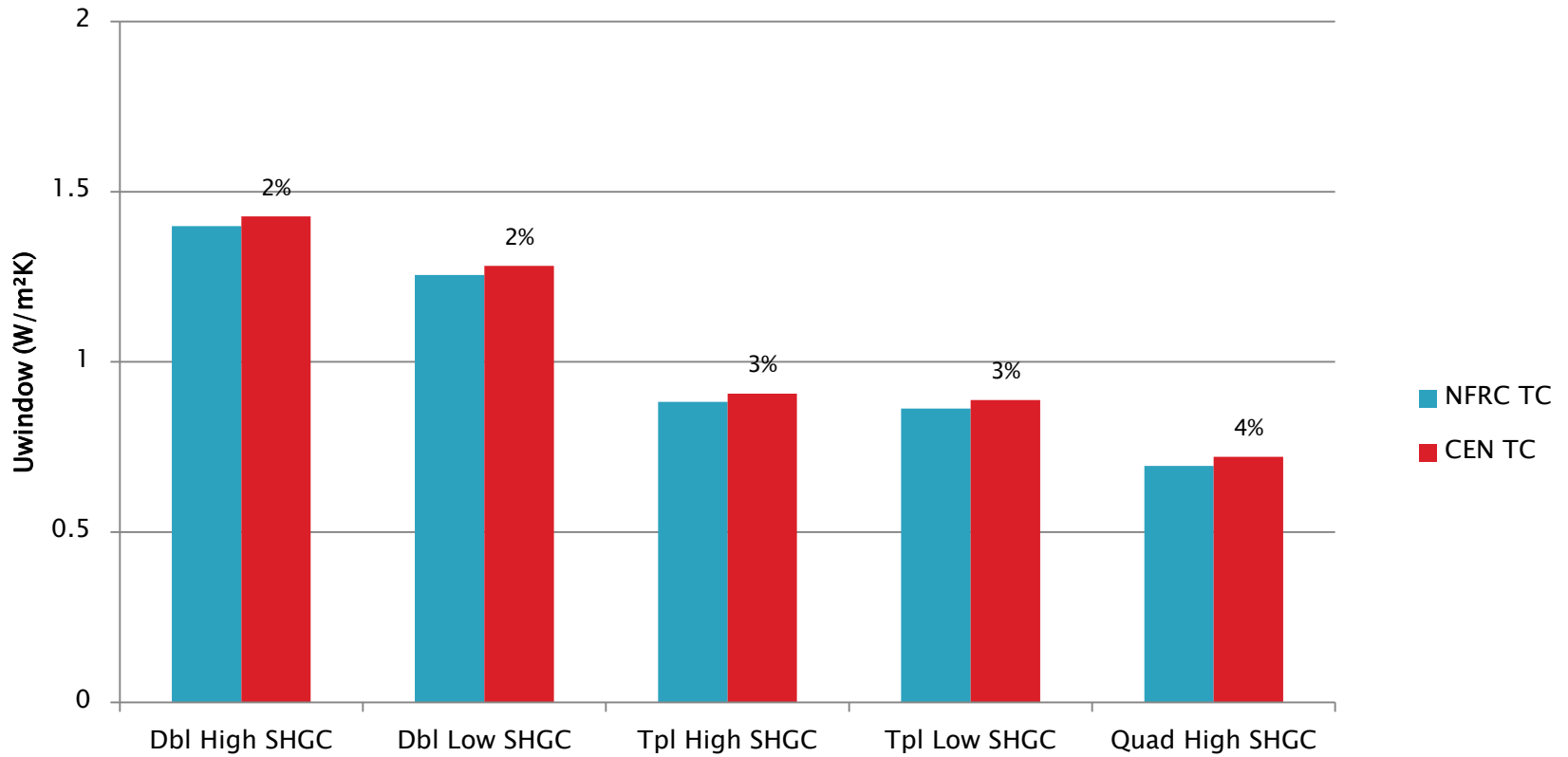
- ▶ The NFRC SHGC values were 24– 46% lower than CEN values (standard methods)
- ▶ NFRC SHGC values were 2–5% higher than CEN values for the triple and quad IGUs (IGU only)



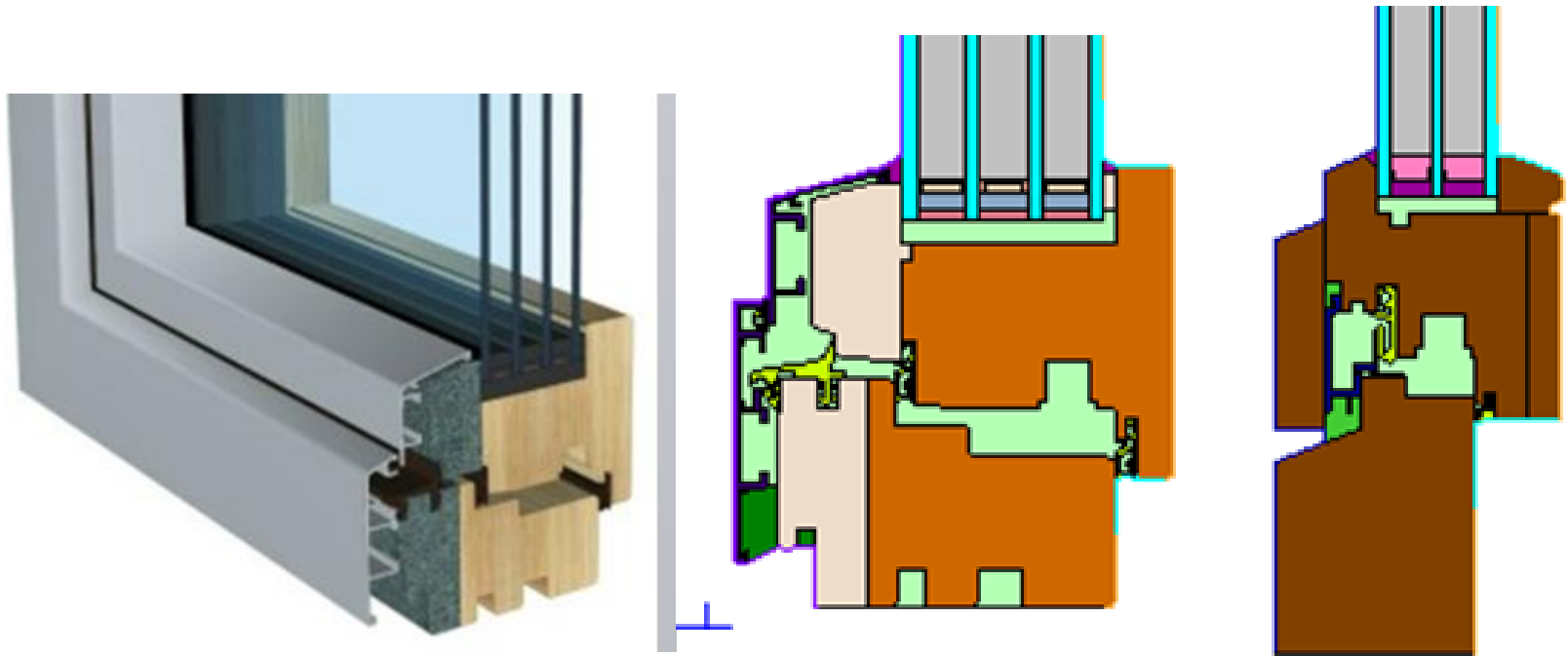
# Center-of-Glazing U-values ( $U_{cog}$ )



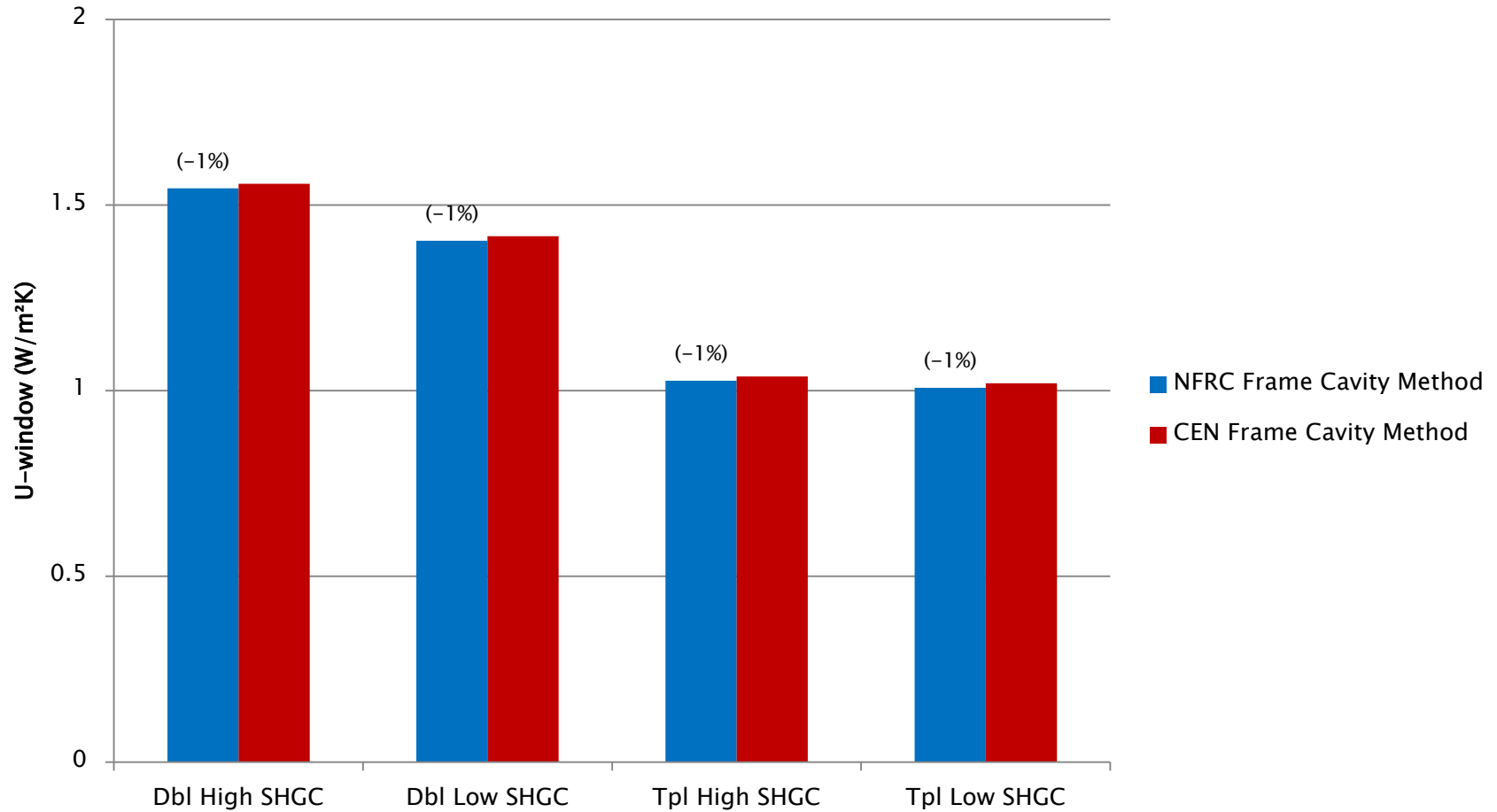
# Material Thermal Conductivities (TBSW)



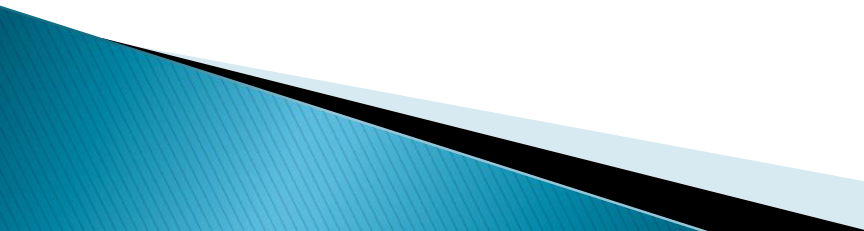
# TBSW vs Solid Wood Windows



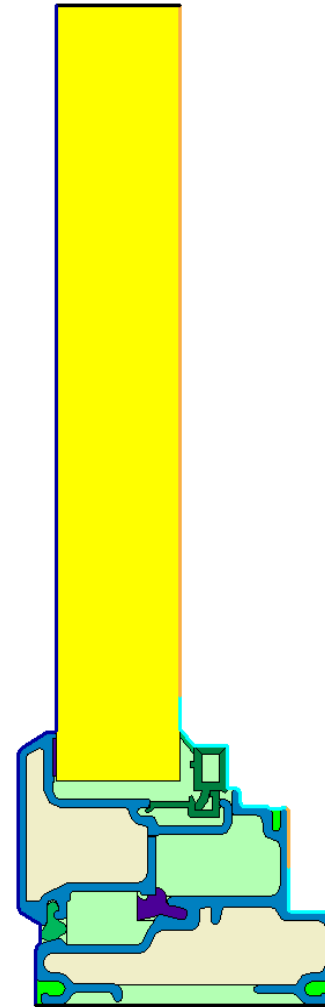
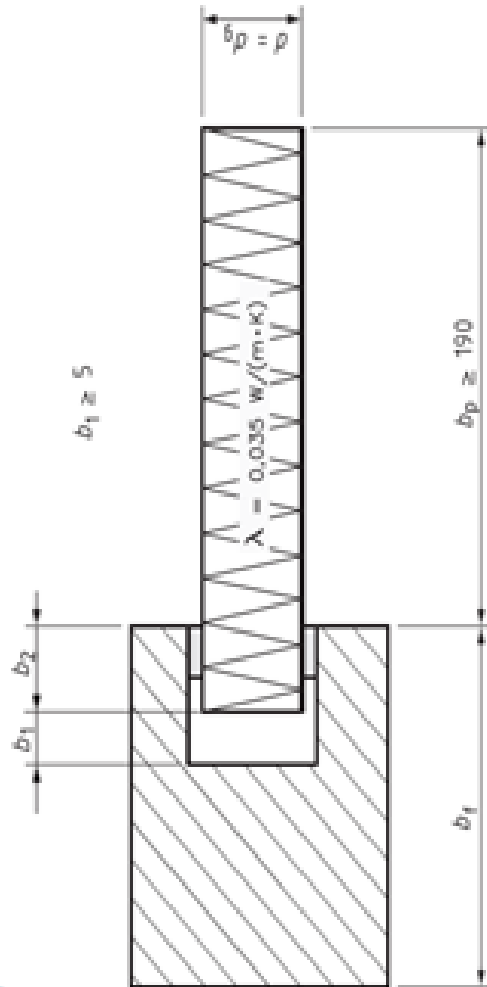
# Frame Cavity Methods (U<sub>window-NFRC</sub>)



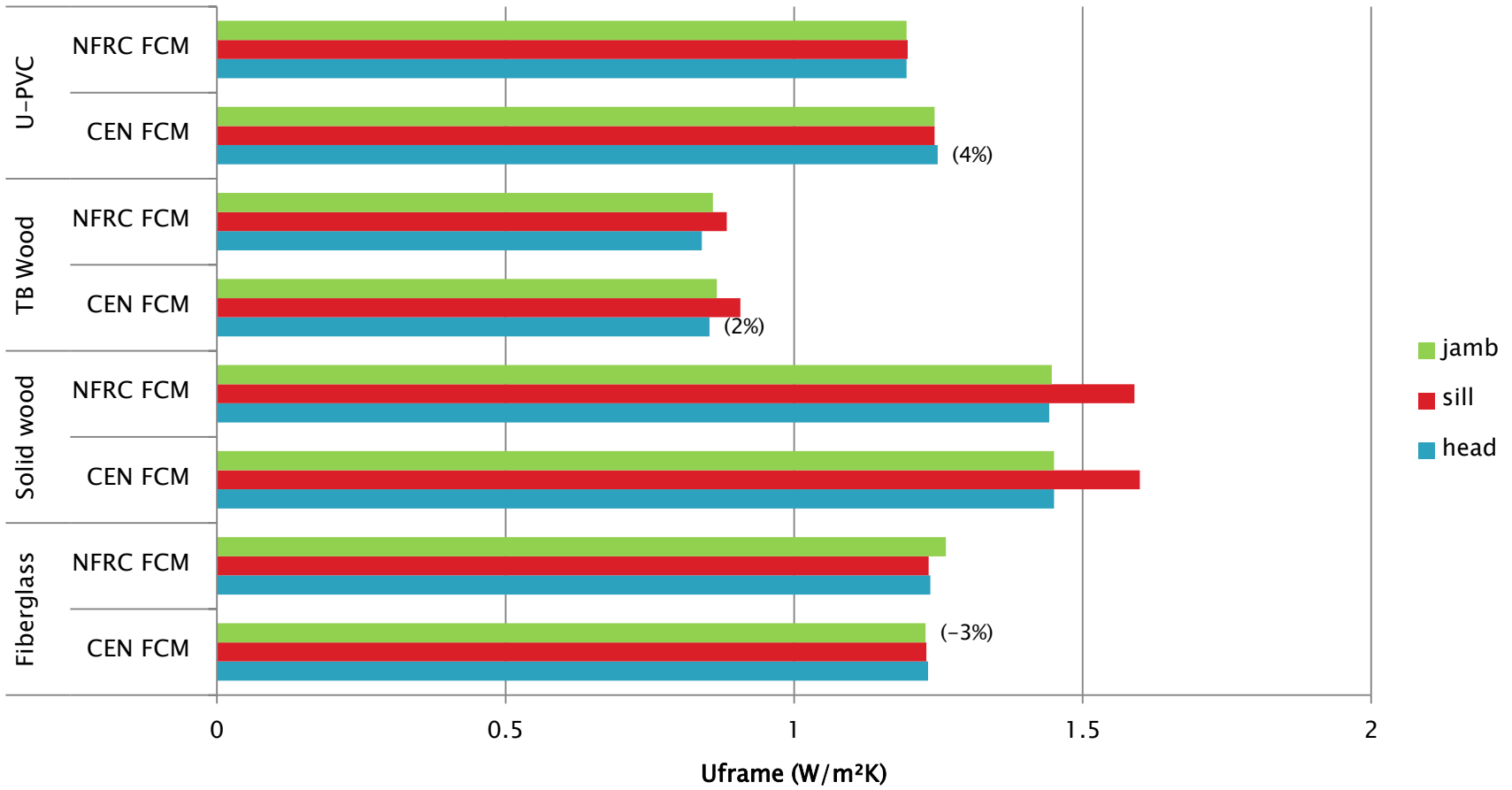
# Surface Film Coefficients

- ▶ Radiation coefficient: cannot be interchanged due to temperature dependent variable
  - ▶ Convective coefficient: no significant difference
  - ▶ Higher surface film coefficients contribute to higher  $U_{\text{window}}$  values
  - ▶ Inland and coastal locations: no significant difference
- 

# $U_{\text{frame-CEN}}$ with Calibration Panel (ISO 10077-2)



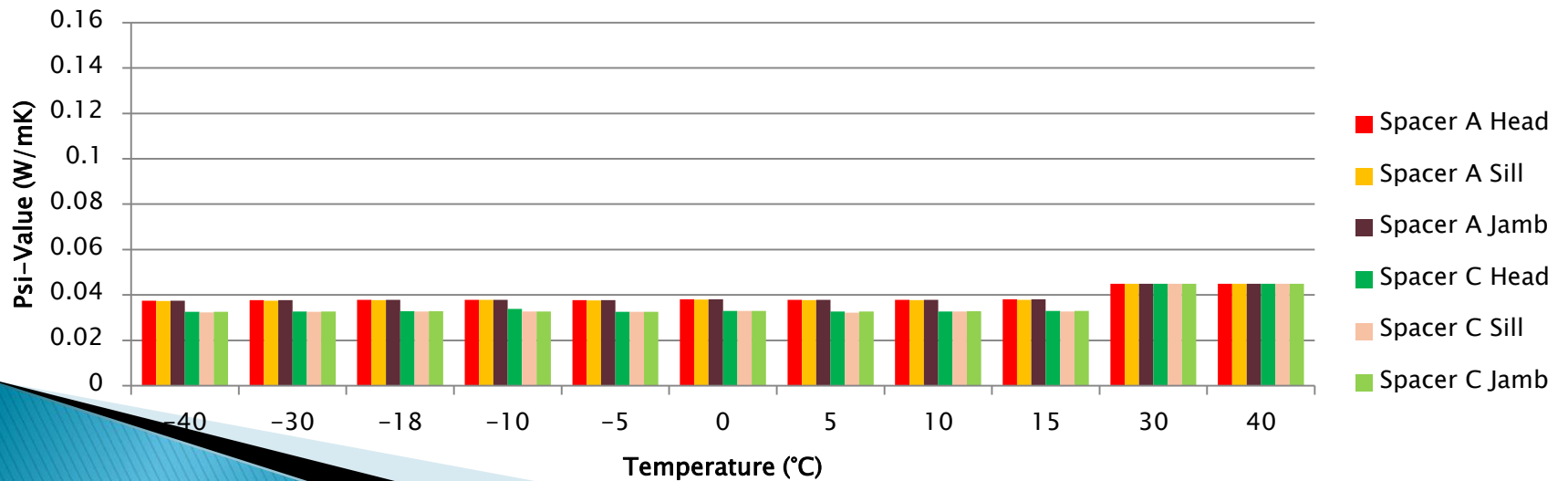
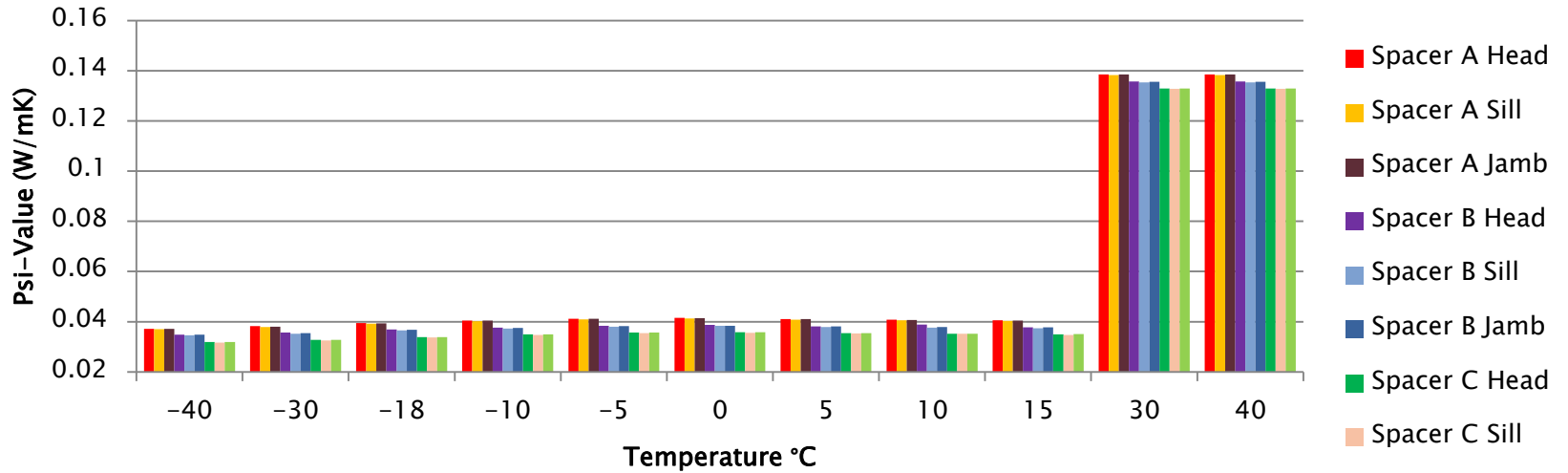
# U<sub>frame-CEN</sub>



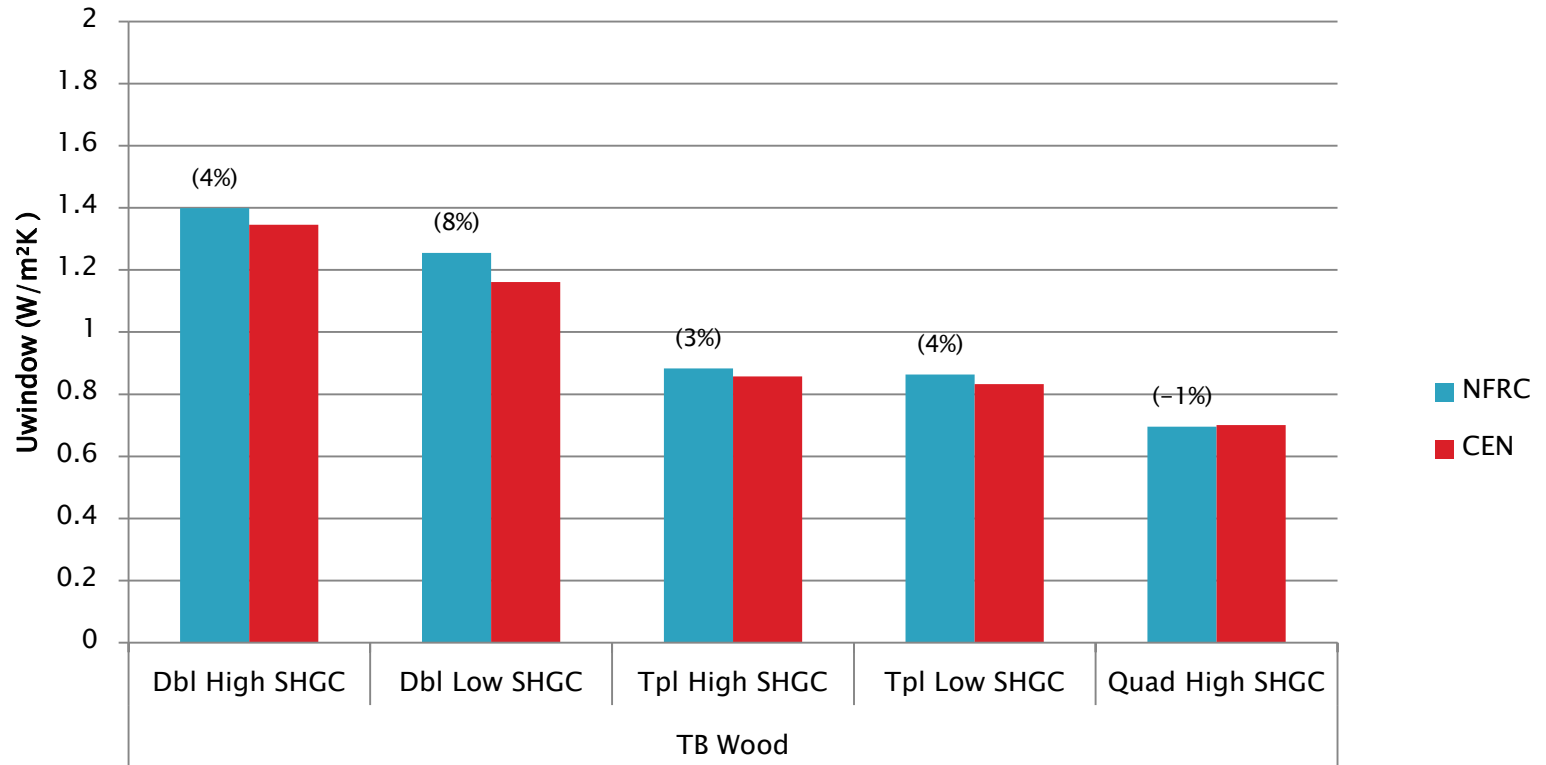


# $\Psi$ -Values

TBSW Frame: Double and Quad IGUs

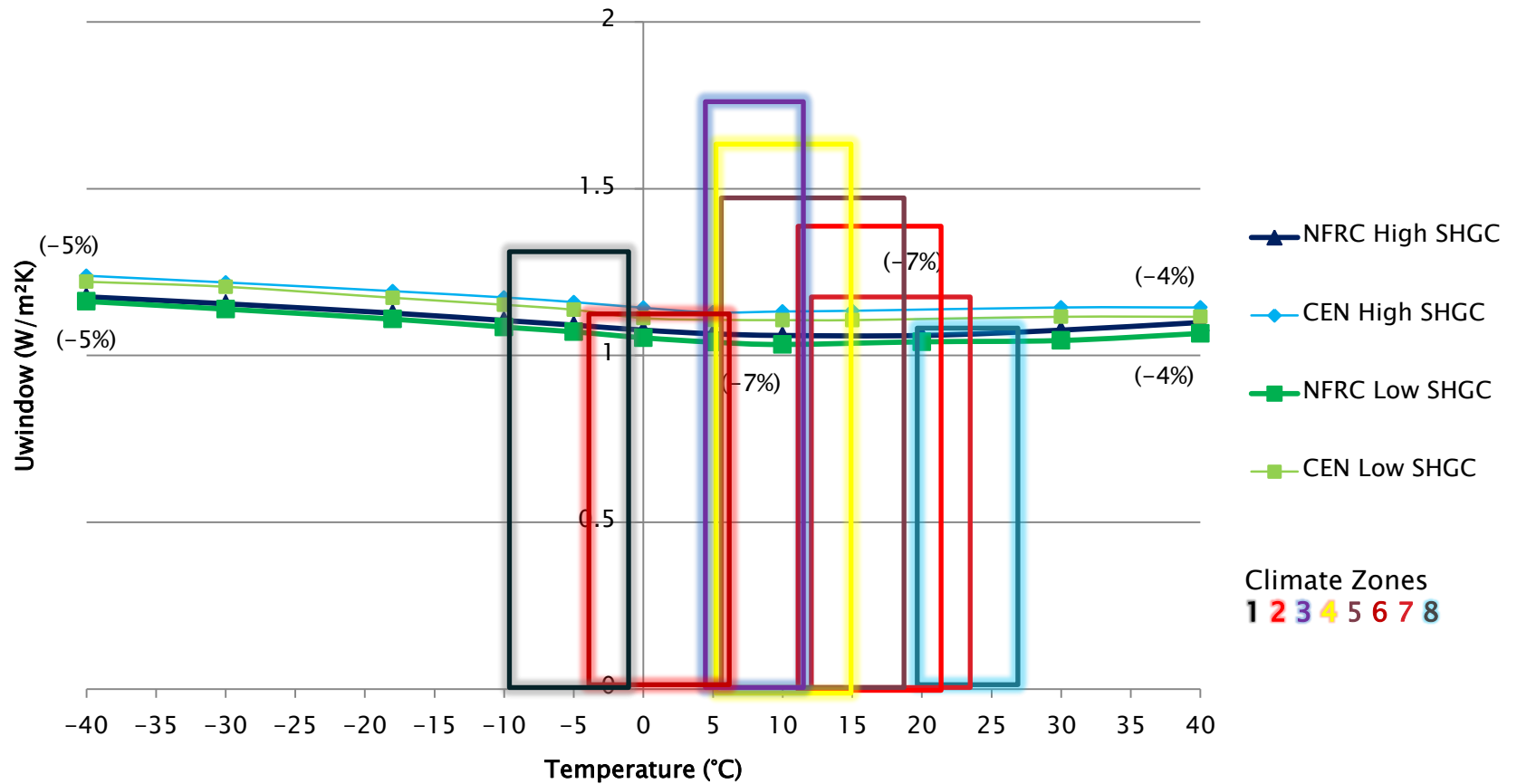


# U<sub>window</sub> Standard Values



TBSW Frame

# $U_{\text{window}}$ in the 8 Climate Zones



Solid Wood, Triple IGU

# Harmonization of Both Methods

- ▶ Exterior temperature symmetry
- ▶ Frame cavity method
- ▶ Material thermal conductivity
- ▶  $U_{\text{frame}}$  method

# Areas that Need Improvement

- ▶ SHGC (with and without the frame)
- ▶ Ucoq method
- ▶ Climate specific U-values
- ▶ Single International Calculation Method  
( $U_{W-ITN'L}$ )

# Questions? Comments?



(Miller, 2010)